

# Corrected Rock Fracture Parameters Applied to Qatari Rock Masses

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# Corrected rock fracture parameters applied to Qatari rock masses Paper ID: XX-XX

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#### **ABSTRACT**

This paper is the continuation of the author's previous publication, Vučemilović et al. (2021), and an attempt to shed light on some of therein presented propositions. In our previous work, we introduced a novel parameter for borehole rock mass evaluation, the FIc, (Fracture Index Corrected) and applied it to Qatari rock masses along with RQDc (Rock Quality Designation Corrected) as described by Li et al. (2009). This was the first case of such wide scale application of these borehole evaluation parameters. A short history is given on alternative proposals by several authors for improvements and amendments of RQD (Rock Quality Designation) since it was proposed by Deere (1963) and Deere and Deere (1988), with their authors' commentaries. Scale considerations are presented for both parameters which are essential consideration factor for any borehole parameter. The paper is concluded with remarks on assumed advantages and limitations of the two parameters and their future research and usage prospects. Paper is concluded with statements that Qatari rock masses are unique type of rock mass which has not been sufficiently researched or classified by the leading world scientists in this field.

**Keywords:** Qatar, Rock masses, Rock mechanics, Corrected Rock Quality Designation, Corrected Fracture Index

#### 1 INTRODUCTION

In this paper, the author has utilized the same data set which was used by Vučemilović et al. (2021) [1], which consisted of exploration data from 201 boreholes spread over the southern regions and suburbs of the city of Doha. An analysis of relationship between RQD and  $\lambda$  (fracture frequency equivalent to FI – Fracture Index, or FF – fracture frequency) parameters shows how Qatari rock masses cannot be compared with a database of world-wide rock masses e.g. from Russo and Hormazabal 2019 [2].



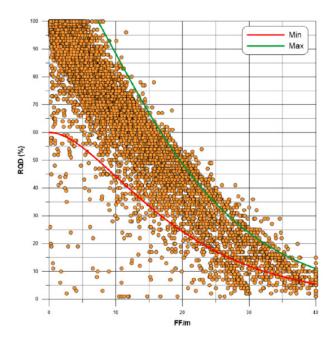


Figure 1: Relation between RQD and mean fracture frequency  $\lambda$  (FF – Fracture Frequency) according to Russo and Hormazabal 2019 [2]

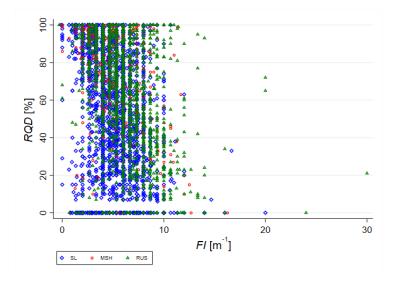


Figure 2: Relation between RQD and frequency  $\lambda$  (FI) for Qatari rock masses

The theoretical relationship between RQD and  $\lambda$  is loosely linear and has been established by Priest and Hudson (1976) [3] as one where RQD tends to decrease with the increase of  $\lambda$  in a more or less a narrow band diagonally. This was confirmed by Russo and Hormazabal (2019) [2] who have collected over 30,000 data points from varied rock mases (figure 1). This is not the case, however, for elaborated Qatari rock masses, which display a different trend in figure 2, where the dependence is also in a (wider) band but vertically down across entire span of RQD values. The graph is differentiated for SL (Simsima limestone), MSH (Midra shale) and RUS (Rus formation) geological members. It can be observed that RUS member assumes minimal RQD values to a lesser extent than

SL member, which is likely owed to the fact that SL layer Weathered Simsima is the most fractured of all layers from all three geological members. Data points for MSH member do not allow any similar conclusions.

Section 2 provides definitions in connection with RQD,  $\lambda$  (FF, FI), RQDc and FIc parameters relevant to this paper. Section 3 gives a review from the existing literature of some proposals on alternative parameters, improvements, and amendments of RQD, as it was originally proposed by Deere (1963) [4] and Deere and Deere (1988) [5], and includes their authors' commentaries on the prospects of their usage. At the end of this section, the most suitable parameter for Qatari rock masses is discussed and chosen. In section 4, scale considerations for both parameters are discussed in detail with conclusions on the applicability of scanning length adjustments of subject parameters for Qatari rock masses, given the maximum core box length utilized in Qatar. The Conclusions section, similarly, discusses the Author's stance on the advantages and limitations of the new parameters and presumed prospects for their further research and usage, and ends with a general commentary on uniqueness of Qatari rock masses in wider terms.

#### 2 DEFINITIONS

RQD is a rock evaluation parameter introduced by Deere (1963) [4] as a parameter of estimation using exploratory boreholes. It is defined as sum of all solid core pieces, which are at least 10 cm long in a core run, divided by the total length of the core run. The equation by Hudson and Harrison (2000) [6] addresses the theoretical relationship between the theoretical RQD ( $RQD^*$ ), fracture frequency  $\lambda$ , and length of the threshold t, which is assumed to have an arbitrary value.

$$RQD^* = 100(t\lambda + 1)e^{-t\lambda} \tag{1}$$

Fracture frequency  $\lambda$  is number of discontinuities in a core run divided by its total length, that is, number of discontinuities per meter of core run.

Li et al. (2009) [7] have proposed a corrected *RQD* parameter, or *RQD*C which is expressed by a formula:

$$RQD_C = \frac{p_r}{N^a} \tag{2}$$

where  $p_r$  is percentage of core recovery, or SCR (Solid Core Recovery), and N is the number of unbroken core pieces in a core run and a is the exponent of a power law function.

Author's proposed corrected FI parameter (FIc) can be defined as (Vučemilović et al. (2021) [1]):

$$FI_C = \frac{100(N-1)}{p_r L} \tag{3}$$

where  $p_r$  is the percentage of recovery, or SCR (0–100), N is the number of cores in a core run, and L is the length of a core run.

#### 3 SOME ALTERNATIVE BOREHOLE FRACTURING PARAMETER PROPOSALS

Azimian (2015) [8] has proposed an improved *RQD* parameter (*RQDI*), which takes into account joint angles and orientations from the *WJD* (Weighted Joint Density) method developed by Haftani et al. (2015) [9] but also considers fractured zones, crushed zones, and void zones (referred to as vuggy or karstic zones). The proposal is presented with the formula

$$RQD_{I} = 100 - \left[100 \frac{f_{i} + CW + Fr + Cr + K}{L_{i}}\right]$$
 (4)

where,  $f_i$  is the value from Haftani et al. (2015) [9], CW is the length of the void, or K washed core segment, Fr is the length of the fragmented core segment (with spacing of 15 – 50 mm), Cr is the length of the crushed core segment (with spacing < 15 mm).  $L_t$  is total core run length.

Araghi et al. (2006) [10] proposed the modified RQD parameter, MRQD. This parameter is obtained by subtracting the weak zone parameter WZ from the value 100.

$$MRQD = 100 - WZ \tag{5}$$

$$WZ = \frac{1.5nd + CW + Fr + Cr + VZ + C}{L_t} \tag{6}$$

Where nd is the number of discontinuities, CW is washed core portion length, Fr is fragmented core portion length, Cr is crushed core portion length, VZ is vuggy core portion length, C is void core portion length, and  $L_t$  is total core run length. The method is very similar to the one introduced by Azimian (2015) [8] but it does not include the joint orientation parameter  $f_i$ .

Ahmed (2013) [11] proposed a modified RQD, which is similar to that of  $RQD_C$ , designated as RQDm. He suggested that the logging session includes the core pieces lesser than 10 cm and lesser than 5 cm, along with those larger than 10 cm.

$$RQDm = \frac{\sum pu}{N^f} \tag{7}$$

$$\sum pu = pu1 + pu2 + pu3 \tag{8}$$

$$f = f1 \times f2 \times f3 \tag{9}$$

where f1 = 1.003 pu1, f2 = 1.001 pu2 and f3 = 0.99005 pu3

and where

pu1 - percentage of core pieces less than 5 cm

pu2 - percentage of core pieces 5 – 10 cm

pu3 - percentage of core pieces > 10 cm

N – number of cores

f – exponent of the power function

The next question raised is; which *RQD* modification is best suited for the rock masses at hand? The author has concluded that the most suitable parameter for estimation of the subject rock masses is the *RQD* corrected, *RQD*<sub>C</sub>, which was proposed by Li et al. (2009) [7].

1. The parameter is simple and does not have a very detailed decomposition of types, length wise, of core run segments;

- 2. Its starting point is  $p_r$ , percentage of recovery, or SCR, as opposed the maximum value of 100 (as proposed for RQDI and MRQD), which is considered a bias;
- 3. Unlike RQDm, the RQDc does not have a fixated exponent value, which proves to be very useful since it lends adjustability.

## 4 SCALE CONSIDERATIONS FOR $RQD_C$ AND $FI_C$

If we consider the data at hand from the Qatari rock masses, we must note the following:

- 1. RQDc and FIc values were calculated, for great majority of data, with 1.5 m scanning interval.
- 2. It would be of interest to develop theoretical dependencies of *RQD*<sub>C</sub> vs *FI*<sub>C</sub>, such as for 1.0 metre scanning intervals.
- 3. Similarly, it would be of interest to present theoretical dependence of *RQD*<sub>C</sub> vs *FI*<sub>C</sub> for different lengths of scanning interval and how this dependence changes for different values of *SCR* parameter.

Figure 3 shows theoretical  $FI_C$  versus  $RQD_C$  for different values of solid core recovery (SCR, or  $p_r$ ). All curves display a logarithmic relationship. The larger the SCR, the lower is the maximum reached  $FI_C$  value. The lesser SCR, the steeper is the increase of  $FI_C$  over smaller  $RQD_C$  spans, and this span gradually shifts toward ever lower  $RQD_C$  values.

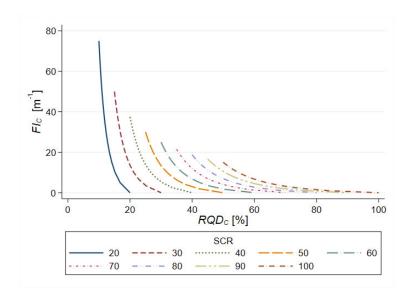


Figure 3: Theoretical variation of  $FI_C$  versus  $RQD_C$ , for different values of SCR and exponent a value (of  $RQD_C$ ) of 0.25, and scanning interval of 1.0 m.

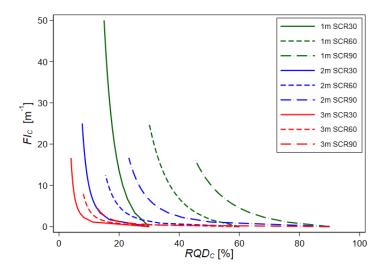


Figure 4: Theoretical variation of  $FI_C$  versus  $RQD_C$ , for different scanning intervals and values of  $SCR_7$  for exponent a value (of  $RQD_C$ ) of 0.25.

In figure 4, the theoretical dependence of  $RQD_{\rm C}$  vs  $FI_{\rm C}$  is shown for three different scanning interval lengths including 1.0 m, 2.0 m, 3.0 m, and SCR values of 30, 60, and 90. We can see overall reduction of  $FI_{\rm C}$  and  $RQD_{\rm C}$  in magnitude and span with increased scanning interval, but within the same scanning interval,  $FI_{\rm C}$  is decreasing and  $RQD_{\rm C}$  is increasing with the increase of SCR. The latter is an identical tendency as in figure 3.

The graphs in figures 5 and 6 display the values of  $RQD_{\rm C}$  and  $FI_{\rm C}$  versus scanning intervals which were given to obtain the borehole core box data. The predominant interval is 1.5 m although it may not be readily visible from the graphs due to the point density. Table 1 shows the percentages of three most frequent scanning interval lengths, over the entire data sets for  $RQD_{\rm C}$  and  $FI_{\rm C}$ .

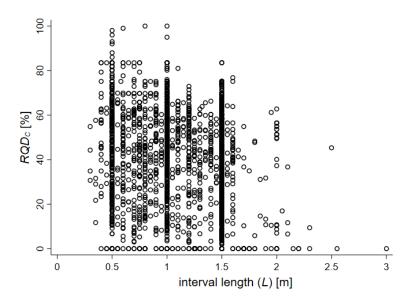


Figure 5: *RQD*<sub>C</sub> values against scanning interval lengths

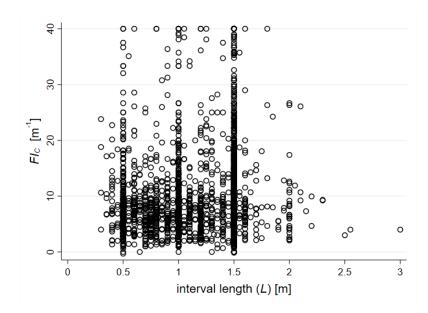


Figure 6: FIc values against scanning interval lengths

Table 1: Proportions of different scanning intervals for *RQD*<sub>C</sub> and *FI*<sub>C</sub>

	L = 0.5  m	<i>L</i> = 1.0 m	<i>L</i> = 1.5 m	L = other
RQDc & FIc				
n	359	627	3314	1363
percentage	6.3 %	11.0 %	58.5 %	24.0 %

### **5 CONCLUSIONS**

RQD is the most frequently used ubiquitous rock evaluation parameter, but obviously it does not work on all rock masses, e.g. on jointed shales as testified by Barton (2021 - personal correspondence). In this paper, a short review is presented on some propositions from the available literature on alternatives to standard ROD by previous authors, along with commentaries from authors which argue against the wide spread usage of their parameters. Author has used these previous proposals to come up with the comparative conclusion on which parameter could be suited for Qatari rock masses. A new corrected parameter was selected and investigated, the RODc together with author's proposed corrected fracturing index  $(FI_C)$ . The  $RQD_C$  parameter applied to Qatari rock masses displays, as opposed to ROD, statistical soundness and accordingly possesses the potential for practical usage and further research. The advantage of using the corrected parameters is their greater sensitivity for detection of fractures ( $ROD_C$  and  $FI_C$ ) and loose core portions ( $FI_C$ ). Possible limitations of the FI<sub>C</sub> parameter are that it can only be used for slightly and moderately weathered rock masses, otherwise it might not be useful for detecting weathered spots within fresher rock masses. Scale considerations were also taken into account for both parameters towards the end of this paper and, as expected, both parameters reduce with scale increase. However, these considerations are warranted only in locations, countries or areas which use core box lengths above 1.5 m, which is maximum length used in Qatar. Minor adjustments at smaller scanning lengths are considered not impactful. Conclusively, Qatari rock masses are a separate "stock" of rock masses not falling under any group of rock masses researched so far by the world's-leading scientists in the field, and as such they possess features worthy of a wider systematic research effort.

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